



LAWRENCE
LIVERMORE
NATIONAL
LABORATORY

A Snowflake Divertor: a Possible Way of Improving the Power Handling in Future Fusion Facilities

D. D. Ryutov, R. H. Bulmer, R. H. Cohen, D. N. Hill, L. Lao, J. E. Menard, T. W. Petrie, L. D. Pearlstein, T. D. Rognlien, P. B. Snyder, V. Soukhanovskii, M. V. Umansky

September 23, 2008

22nd International Fusion Energy Conference
Geneva, Switzerland
October 13, 2008 through October 18, 2008

Disclaimer

This document was prepared as an account of work sponsored by an agency of the United States government. Neither the United States government nor Lawrence Livermore National Security, LLC, nor any of their employees makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States government or Lawrence Livermore National Security, LLC. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States government or Lawrence Livermore National Security, LLC, and shall not be used for advertising or product endorsement purposes.

A Snowflake Divertor: a Possible Way of Improving the Power Handling in Future Fusion Facilities

D.D. Ryutov¹, R.H. Bulmer¹, R.H. Cohen¹, D.N. Hill¹, L. Lao², J.E. Menard³, T.W. Petrie²,
L.D. Pearlstein¹, T.D. Rognlien¹, P.B. Snyder², V. Soukhanovskii¹, M.V. Umansky¹

¹ Lawrence Livermore National Laboratory, Livermore, CA 94551, USA

² General Atomics, San Diego, CA 92186, USA

³ Princeton Plasma Physics Laboratory, Princeton, NJ 08543, USA

Abstract

Handling high power loads on plasma facing components is one of the critical issues in developing an economically competitive fusion reactor based on tokamak. In this study, we provide a detailed analysis of a relatively unexplored approach to this problem based on the use of divertors with the poloidal magnetic field structure closely approaching a second-order null. We demonstrate that this geometry opens up new possibilities for radiative divertors, has favorable effect on the convective transport, and provides an additional control over ELM activity. In the ideal case where the null is exactly second order, the separatrix near the null acquires a characteristic hexagonal shape reminiscent of a snowflake, whence the name of this configuration. It can be created by a simple set of divertor coils situated outside the toroidal field coils.

1. Introduction

Handling high power loads on plasma facing components is one of the critical issues in developing an economically competitive fusion reactor based on tokamak. The optimal choice of a heat-load mitigation problem for a given device will be made based on a variety of considerations, including details of plasma equilibrium, life-time and maintainability of in-vessel components, the complexity of the magnetic system, and many others. The decision can be made only on the basis of an integrated design, which is still in the future. So, parallel research into several approaches seems quite reasonable now.

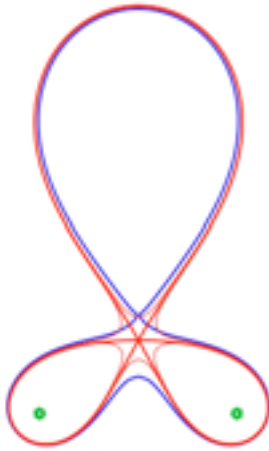


Fig. 1 Separatrix for the exact second-order null (thick red line) and the nearby flux surface (thin red line). Separatrix for the snowflake-plus configuration is shown in blue. The divertor coils are shown in green dots.

In this paper we consider the “snowflake” (“SF”) divertor configuration, first described in Refs. [1, 2]. This divertor exploits a tokamak geometry in which the poloidal magnetic field null approaches second order; the name stems from the characteristic hexagonal, snowflake-like, shape of the separatrix for an exact second-order null (Fig. 1). The poloidal magnetic field in this latter case is a quadratic function of the distance to the null, whereas in the standard X-point configuration it is a

linear function. This means that the flux expansion is much larger in the vicinity of a null of a snowflake divertor, and one can try to exploit this fact for reducing the divertor heat load.

When using the terms “X-point divertor” or “standard X-point configuration”, we mean a configuration with an X-shaped separatrix near the null point. This should not be confused with the recently proposed “X-divertor,” where additional coils cause significant reduction of the magnetic field in the divertor legs at some distance from the X-point [3], and the even more recent “super-X divertor” [4], where further reduction of the heat load is expected to occur due to

a significant increase of the major radius and thus available surface area in the outer strike-point region.

The SF configuration can be created by a simple set of divertor (poloidal field) coils (an example is shown in Fig. 1), having currents I_d related in a certain way to the plasma current [1]. The distance from the divertor coils to the null-point is approximately equal to the plasma minor radius. For large facilities, this allows placing divertor coils outside toroidal field coils.

Typically, the current I_{d0} that makes an exact second-order null is of order of the plasma current I_p . If the current in the divertor coils is higher than I_{d0} , the configuration becomes an X-point configuration, but with a small gradient of the poloidal field near the null-point. We call this configuration a “snowflake-plus” (Fig. 1). Its advantage is that it is remarkably robust with respect to possible un-controlled variations of the plasma current [1,2]. For a current I_d that is lower than I_{d0} , two X-points appear on the separatrix. We call it a “snowflake-minus” configuration [1,2]. Our main emphasis here is on the snowflake-plus configuration.

2. General properties of a snowflake configuration

In Ref. [1] it was pointed out that exact snowflake configuration is topologically unstable, and that it might be beneficial to operate the divertor in the aforementioned “snowflake-plus” mode, where the current I_d in divertor coils is somewhat higher than the one that corresponds to an exact snowflake configuration. In this case, if the configuration remains symmetric with respect to the $x=0$ plane, the expansion of the flux function near the null point acquires the form:

$$\Phi = \frac{I}{c} \left[\eta z + \frac{A}{r_e^2} \left(x^2 z - \frac{z^3}{3} \right) \right] + C, \quad (1)$$

where x and z are a horizontal and vertical coordinates in the poloidal plane of Fig. 1, r_e is the distance between the magnetic axis and the separatrix in the equatorial plane (roughly, the plasma minor radius), the constant A of order unity depends on details of the geometry of PF coils, and constant η characterizes the proximity to an exact snowflake. In the simple model shown in Fig 1 it is merely

$$\eta \equiv (I_d - I_{d0}) / I_{d0}. \quad (2)$$

The constant C is determined by the condition that the poloidal magnetic flux be zero ($\Phi=0$) on the separatrix. In the exact snowflake configuration this constant is zero.

The distance between some magnetic surface and the separatrix near the magnetic field null increases significantly compared to that distance in the equatorial plane of the device. A key characteristic of this flaring effect is the minimum distance between the null-point and a magnetic surface, Δ_0 , compared to the distance Δ_e between this magnetic surface and the separatrix near the equatorial plane. The larger the ratio

$$F \equiv \Delta_0 / \Delta_e, \quad (3)$$

the stronger the flaring. Another way of characterizing the flux expansion is comparing the minimum of the poloidal magnetic field on a certain flux surface, B_{Pmin} , to the value of the poloidal field in the equatorial plane, B_{Pe} . The corresponding ratio is denoted by $G \equiv B_{Pe} / B_{Pmin}$. Both F and G are presented in Fig. 2 for the snowflake divertor (S subscript) and the standard X-point divertor (X subscript), for a similar overall plasma shape. One sees that, indeed, the SF configuration provides significantly stronger flux expansion than the standard one.

Another benefit of the snowflake geometry is related by its effect on the magnetic shear just *inside* the separatrix, in the pedestal region. We define the magnetic shear in the vicinity of the separatrix as

$$S = r_e dq/d\Delta_e, \quad (4)$$

where q is a standard safety factor, and Δ_e is defined before Eq. (3). The magnetic shear is shown in Fig. 3. One sees that, by a mere 5% variation of the current in the divertor coils, one can significantly change the shear in the pedestal region. This may provide a useful tool for the control over the peeling-ballooning instability that is thought to play a significant role in the behavior of ELMs [5,6].

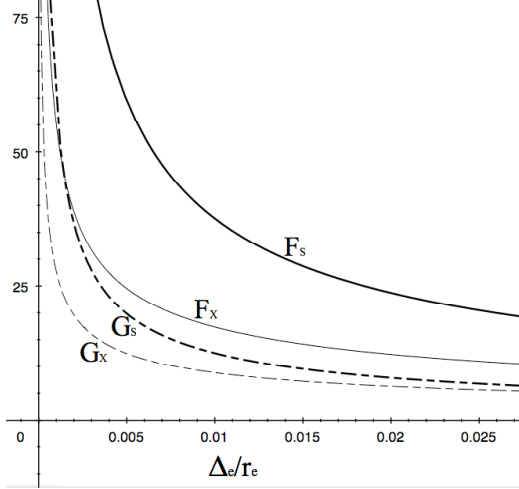


Fig. 2 Geometrical expansion parameters for a snowflake (bold line) and X-point configurations (thin line). The parameter r_e is the distance from the magnetic axis to the separatrix in the equatorial plane. At the boundary of a typical SOL, one has $\Delta_e/r_e \sim 0.01 - 0.003$, so that the ratio F_s/F_x is in the range of 1.5-3. Dashed lines represent the magnetic expansion parameter G . The ratio G_s/G_x is in the range 1.5-2.

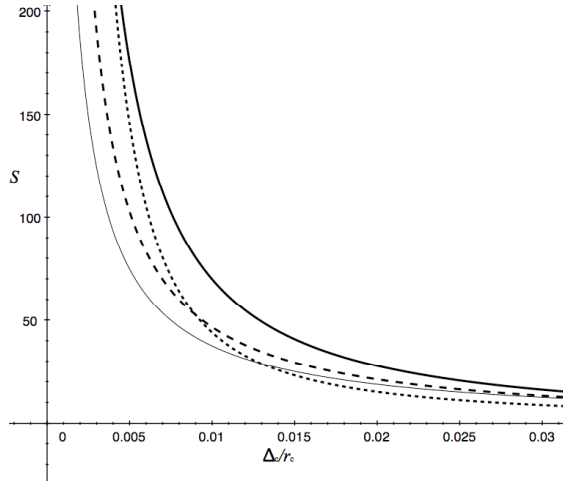


Fig. 3 Magnetic shear for the standard X-point divertor, thin line, and for the snowflake-plus divertor, thick lines. Solid line: $\eta=0$ (an exact snowflake), $\eta=0.025$ (dashed line) and $\eta=0.05$ (dotted line). Large values of the parameter S are related to the normalization. More important is the change of the S profile for the snowflake divertor compared to that of a standard divertor: in the immediate vicinity of the separatrix, the snowflake-plus divertor yields higher value of S , whereas at some distance from the separatrix, deeper into the pedestal region, S can become both larger and smaller than for the X-point divertor. This can be used to control ELM activity.

The magnetic shear outside the separatrix causes a stronger squeezing of the magnetic flux tubes passing near the magnetic null point than for the standard divertor. The shear will have a strong effect on the SOL turbulence (see Sec. 5 below).

3. Snowflake in specific devices

In some cases, the snowflake configuration can be created on existing devices, with the use of only existing poloidal field coils. We have looked into this possibility for the DIII-D tokamak at General Atomics. Figure 4 shows the CORSICA [6] equilibrium reconstruction for a shot with a plasma current of 1 MA. This figure corresponds to the parameter $\eta \sim 0.03$. Importantly, the plasma current in any each PF coil does not exceed its coil current-carrying capacity.

The snowflake geometry is also compatible with spherical tori. Figure 5 shows a possible snow-flake-plus configuration for the proposed high-heat-flux facility at PPPL [8]. Figure 6

shows the transition from the snowflake-plus to the snowflake-minus geometry with the NSTX spherical torus. The change from SF-plus to SF-minus configuration required only 10% change in the current distribution between PF coils. Figures 5, 6 were obtained based on the ISOLVER code [9].

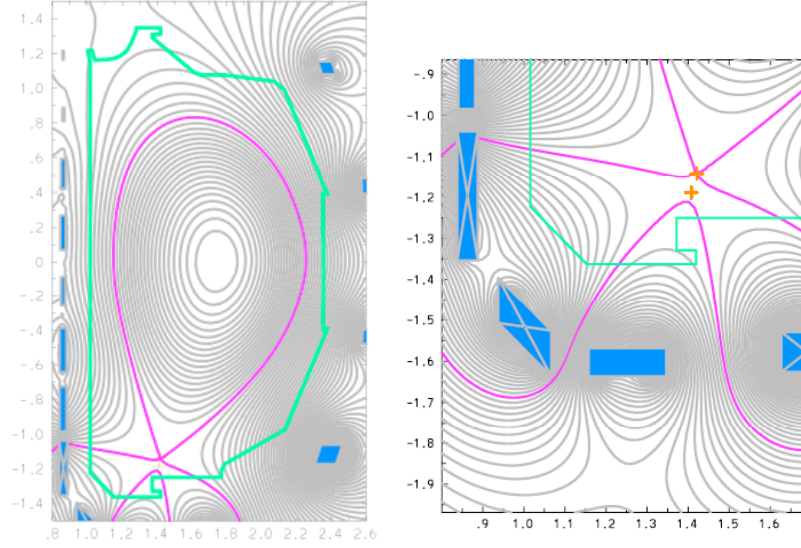


Fig. 4. Snowflake configuration for the DIII-D tokamak. Left panel: general view of the poloidal cross-section; right panel: blow-up of the divertor region. Shown in blue are poloidal field coils; separatrix is shown in pink. Plasma current 1 MA. Configuration corresponds to the snowflake-plus geometry with the parameter $\eta \sim 0.03$.

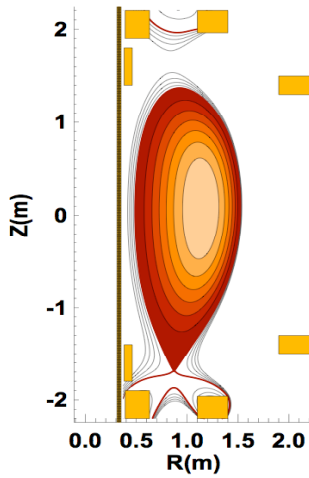


Fig. 5 A snowflake-plus configuration for the proposed high-heat-flux spherical torus NHTX (PPPL).

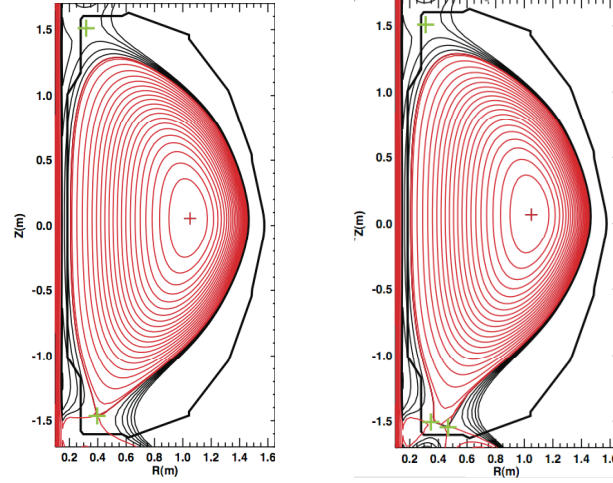


Fig. 6 A snowflake-plus (left panel) and snowflake-minus (right panel) configurations for the NSTX spherical torus (PPPL). Note the appearance of two closely spaced nulls in the second case (light-green dots).

4. First UEDGE simulations.

The Fusion Development Facility [10], aimed at neutron and other testing of the reactor components, will have to handle high energy fluxes in the divertor. We have applied the UEDGE code [11] to assess possible benefits of the snowflake geometry for the anticipated parameters for the FDF facility. Fig 7 shows the comparison of the magnetic field structure for the X-point geometry (left panel) and snowflake-plus geometry (right panel). Note that the shape of the separatrix doesn't change significantly above the level of $z \sim 1$ m, implying that the transition to

the snowflake geometry would not have a significant direct effect on the core plasma performance. Despite the fact that the divertor plates in the snowflake case were situated at a very similar magnetic field, the change in the geometry has lead to significant changes in the profile of plasma parameters near the divertor plates (with plasma parameters in the upper SOL being essentially the same); Fig. 8 illustrates this statement.

Addition of 1% of Argon gives rise to a significant reduction of the heat load on the outer divertor. In a typical case the heat load (in the presence of 1% of Ar) was roughly 2 times less in the snowflake case than in the standard case. The effect of the configuration on the heat flux on the inner divertor was less significant. In some cases, the “inner” heat flux in the snowflake geometry was larger than in a standard geometry, although it was less than the heat flux on the outer plate.

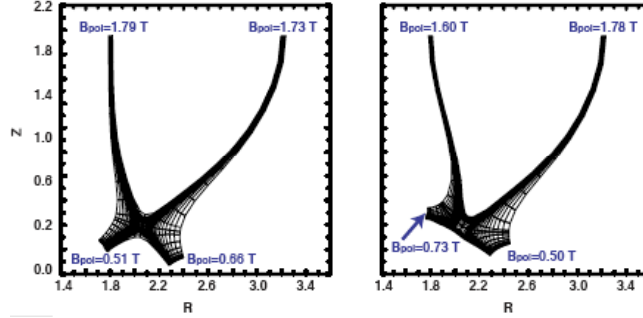


Fig. 7. Possible magnetic field structure for the FDF facility: standard X-point (left panel) and snowflake-plus (right panel). Values of B_{pol} in the midplane and at the divertor plate are indicated.

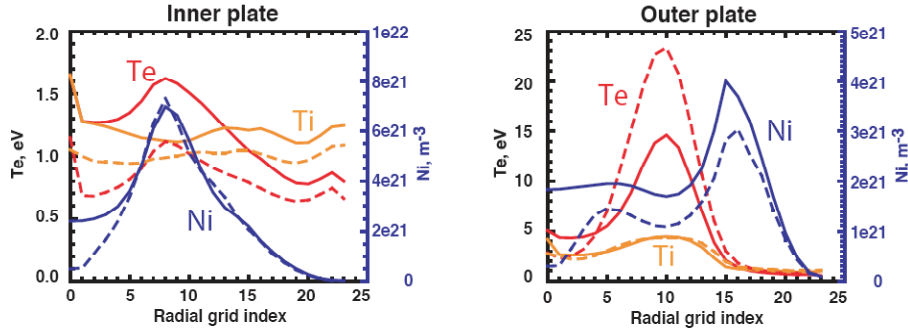


Fig. 8 UEDGE results for the FDF geometry. Solid lines – snowflake geometry; dashed lines – standard X-point geometry. There was no impurity radiation included. Note a significant reduction of the electron temperature.

5. Preventing divertor turbulence from propagating into main SOL

In the open field line region, the plasma pressure is typically small, and plasma turbulence is dominated by flute-like structures aligned with magnetic field lines. The dynamics of such structures is significantly affected by the presence of a magnetic field null and associated squeezing of the flux-tubes [11, 12]. In this section we describe squeezing in the snowflake geometry and find that it is much stronger than in the case of a standard X-point divertor.

Consider a flux tube whose cross-section is circular at some point in the divertor region (Fig. 9). Tracing this fluxtube towards the vicinity of the null point and further to the main SOL, one finds that the cross-section is squeezed and becomes elliptic, very much as for a standard X-point divertor [11]. We denote the minor and major semi-axes of the fluxtube cross-section as w_{minor} and w_{major} . It is assumed that the cross-section is small enough that w_{major} does not exceed the length-scale of the magnetic field. As the flux through the cross-section remains the same along the length of the flux tube, and the field strength does not vary significantly, the product of

$$E = \frac{w_{major}}{w_0} > 1, \quad (5)$$

Based on the results of Ref. [2], one can show that, for a flux tube circular at point “0”, the ellipse at point “1” becomes tilted by an angle of approximately 40° with respect to the flux surface, and elongation becomes

$$E_1 \approx 1.57 \frac{l_D^2}{\Delta_0^2}, \quad (6)$$

The presence of the flux-tube squeezing prevents the divertor-leg turbulence from extending to the main SOL (this circumstance will be used in the next section). Indeed, even for a modest value of $l_D=3\Delta_0$ the elongation E_2 becomes ~ 150 . This means that the perturbations, whose perpendicular scale-length in the divertor is as large as 100 ion gyro-radii, become squeezed to a size less than the ion gyro-radius as they are mapped to the main SOL. This, in turn, means that the plasma turbulence in the divertor is decoupled from that in the main SOL.

Reduction of the magnetic field in the strike point is a measure of the poloidal flux expansion and of the corresponding increase of the wetted area for a given SOL width. We measure the width in terms of the e-folding length Δ_e of various quantities in the tokamak equatorial plane (Δ_e may be different for these various quantities). The poloidal field flux through the SOL in the equatorial plane is $2\pi B_{Pe} R \Delta_e$. Assuming that the poloidal flux threading the SOL does not change between the midplane and divertor (possible deviations from this assumptions are considered later in this section), one finds the wetted area on the divertor plate, $(2\pi R \Delta_e) B_{Pe}/B_{PD}$. Obviously, the surface area is larger for a weaker poloidal field at the strike point (Cf Sec. 2).

Further increase of the wetted area can be achieved by tilting the divertor surface so as to make the angle α between the poloidal magnetic field and divertor surface small (Fig. 10). This, obviously, yields additional large factor $1/\sin\alpha$ in the wetted surface area:

$$S_W = 2\pi R \Delta_e B_{Pe} / (B_{PD} \sin\alpha). \quad (7)$$

However, this approach has its limits, associated with engineering constraints. What may actually be a limitation is the angle between the full magnetic field vector and the surface [13]. As the poloidal field B_{PD} at the divertor plate is small compared to the toroidal field, B_{TD} , the angle γ between the surface and the full vector is

$$\gamma \approx B_{PD} \sin\alpha / B_{TD} \ll \alpha. \quad (8)$$

Possible imperfections in the alignment should be compared with this angle, not α . The, it is obvious that that the wetted area is limited to

$$S_W = 2\pi R \Delta_e B_{Pe} / (B_{PD} \sin\alpha) < 2\pi R \Delta_e B_{Pe} / (B_{TD} \gamma_{\min}). \quad (9)$$

Remarkably, S_W does not depend on the poloidal field at the strike point (B_{PD}).

This result suggests the following approach: use a strong flux expansion in the vicinity of the null-point to radiate a maximum possible power, and then tilt the divertor plate in the recompression zone, as shown in Fig. 10, to reach the largest-possible wetted area (9). The use of relatively long divertor “legs”, with l_D (Fig. 10) large compared to the size of the expansion zone Δ_0 near the null-point opens up the possibility of further spreading of the plasma flow by virtue of enhanced turbulence in the divertor legs [13]. The turbulence is sensitive to the tilt angle α and can be substantially enhanced by making small α .

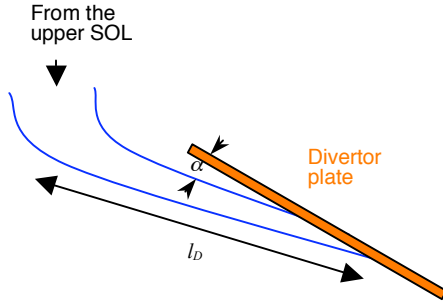


Fig. 9 The geometry of a “long-legged” snowflake divertor (the outer leg). Only part of the divertor plate is shown (the one containing wetted area). Other material surfaces used as baffles, limiters, etc are not shown. Shown in blue are two flux surfaces. The major axis is to the left.

The turbulence induced in the divertor legs does not penetrate to the main SOL because of the strong squeezing of the flux-tubes passing near the magnetic null (Sec. 5). Therefore, the enhanced divertor-leg turbulence does not lead to degradation of the confinement of the core plasma. Note that, under realistic conditions, the length of the divertor legs is significantly smaller than the distance from midplane to the null-point. Accordingly, heat parallel convection/conduction in the divertor takes less time than in the main SOL. Therefore, in order to produce strong plasma expansion in the divertor leg, cross-field transport should be much stronger here than in the main SOL. But the two regions are decoupled from each other (see Sec. 5), and significant difference in transport coefficients may be possible.

In order to further reduce heat flux at the divertor targets, one can consider increasing the radiated power near the divertor target surfaces [14] by puffing impurities directly into the “closed” divertor; the escape of the impurity ions into the main plasma would be inhibited by the enhancing the flow of deuterium toward the divertor plates, e.g., “puff-and-pump”. We leave detailed assessment of this scenario for future work.

7. Discussion.

We have provided a brief discussion of the properties of a snowflake divertor. The set of coils required to generate the snowflake configuration is quite simple. The distance from the

coils to the magnetic null is large, thereby allowing placement of the coils outside toroidal field coils. The snowflake-plus configuration allows one to combine the robustness of the standard X-point configuration and large flux expansion typical of the snowflake geometry. It is quite robust with respect to possible uncontrolled variations of the plasma current.

In addition to the obvious effect on the flux expansion near the null point (typically, by a factor of 2-3 compared to the standard X-point configuration), the snowflake divertor provides additional degree of control over a variety of processes in the scrape-off-layer and in the pedestal region. In particular, the snowflake allows one to control the magnetic shear in the pedestal region just inside the separatrix, thereby providing a tool for affecting ELM activity. The snowflake leads to a stronger squeezing of the magnetic flux-tubes passing near the magnetic null point, thereby affecting divertor-leg instabilities and instabilities in the vicinity of the null-point.

Because of a strong flux expansion, the snowflake increases the SOL volume. Therefore, it holds promise for improved operation in the radiative mode. If divertor legs are long enough, one can try to increase divertor cross-field transport and induce additional spreading of the plasma in the divertor area.

Acknowledgments

Prepared by LLNL under Contract DE-AC52-07NA27344; research at GA was supported by U.S. DoE contract DE-FC02-04ER-54698; research at PPPL was supported by U.S. DOE contract DE-AC02-76-CH03073.

References.

1. D.D. Ryutov. Phys. Plasmas, **14**, 064502 (2007); Erratum: Phys. Plasmas, **15**, 069901 (2008); D.D. Ryutov. Paper D1.002, 34th EPS Conf. on Plasma Phys, Warsaw, 2007 (<http://epsppd.epfl.ch/Warsaw/start.htm>).
2. D.D. Ryutov, R.H. Cohen, T.D. Rognlien, M.V. Umansky. Phys. Plasmas, **15**, 092501 (2008).
3. M. Kotschenreuther, P.M. Valanju, S.M. Mahajan, J.C. Wiley. Phys. Plasmas, **14**, 072502 (2007).
4. M. Kotschenreuther, P.M. Valanju, S.M. Mahajan. “*High Power Density Experiment (HDPX) – A Next Step Device in the Age of ITER.*” Paper 1C presented at the 2008 Intern. Fusion Theory Conf, Boulder, CO, March 31-April 2, 2008.
5. P.B. Snyder, H.R. Wilson, J.R. Ferron, L.L. Lao, A.W. Leonard, T.H. Osborne, A.D. Turnbull, D. Mossessian, M. Murakami, X.Q. Xu. Phys. Plasmas, **9**, 2037 (2002)
6. A.J. Webster, C.G. Gimblett. “The Ideal Magnetohydrodynamic Peeling Mode Instability,” Paper 3B03, International Sherwood Fusion Theory Conference, Boulder, CO, 31 March – 2 April 2008; A.J. Webster, C.G. Gimblett. 34th EPS Conference on Plasma Phys. Warsaw, 2-6 July 2007, ECA Vol. 31F, P-4.088.
7. L.D. Pearlstein, R.H. Bulmer, T.A. Casper, E.B. Hooper, R.A. Jong, T.B. Kaiser, L.L. LoDestro, H.L. Berk, “*Predictive Modeling of Axisymmetric Toroidal Configurations,*” Proc. of the 28th EPS (June, 2001), Funchal, Madeira, and references therein.
8. R.J. Goldston, J. Menard, J.P. Allain, J.N. Brooks, et al. Poster GP6.00125, 50th Annual Meeting of the Division of Plasma Physics, November 17–21, 2008, Dallas, Texas.
9. J. Menard. ISOLVER code, PPPL.
10. R.D. Stambaugh, V.S. Chan, A.M. Garofalo, J.P. Smith, C.P.C. Wong, Poster TP6.00049; A.M. Garofalo T.W. Petrie, J.P. Smith, M.R. Wade, et al. Poster TP6.00051; 50th Annual Meeting of the Division of Plasma Physics, November 17–21, 2008 Dallas, Texas.;

11. T.D. Rognlien J.L. Milovich, M.E. Rensink, G.D. Porter. J. Nucl. Mat., **196-198**; 347 (1992).
12. D.Farina, R.Pozzoli, D.D. Ryutov. Nuclear Fusion, **33**, 1315 (1993).
13. R.H. Cohen, B. LaBombard, L.L. LoDestro, T.D. Rognlien, D.D. Ryutov, J.L. Terry, M.V. Umansky, X.Q. Xu, S. Zweben. Nucl. Fusion, **47**, 612 (2007).
14. A.S. Kukushkin. Private comm. to D.D. Ryutov, July 2007.
15. T.W. Petrie, M.R. Wade, N.H. Brooks, M.E. Fenstermacher et al. J. of Nucl. Mat., **363-365**, 416 (2007).